

1. VEŽBA

1. ZADATAK

Terenskim opitom pomoću standardne kružne ploče prečnika 30.5cm, na dubini od $D_f=1.0\text{m}$, dobijen je modul reakcije k_O (MN/m^3). Nivo podzemne vode je na dubini od 6.0m. Ispitano tlo je homogenog sastava do dubine od 8.00m, a sastoji se od sloja:

- prekonsolidovane gline
- srednje zbijenog, peska

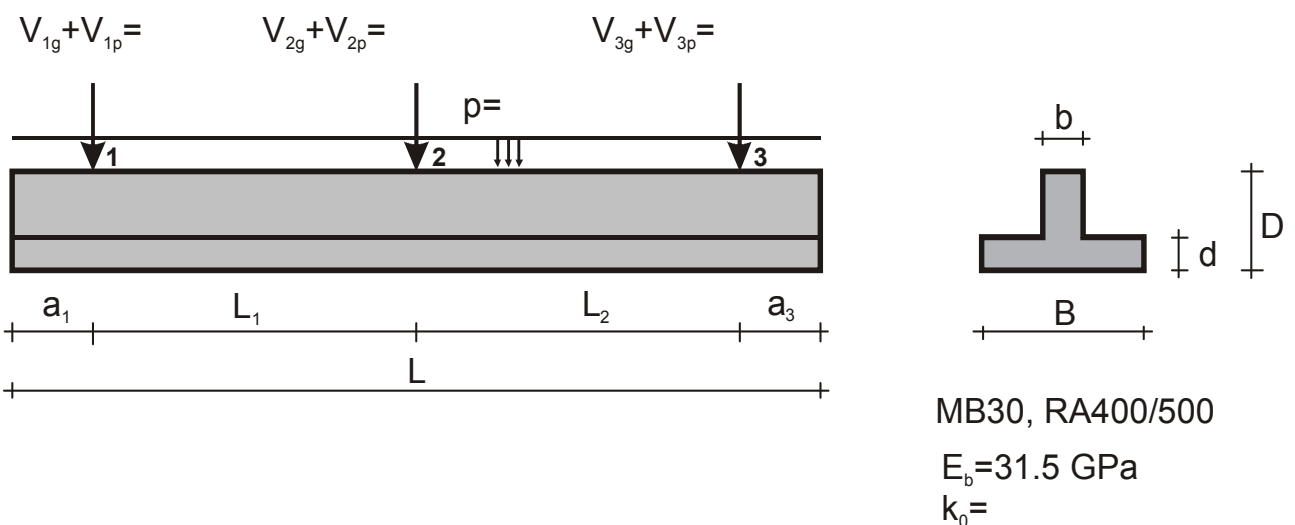
Odrediti ekvivalentni modul reakcije podlog $k=f(k_o, L/B)$, za proračun temeljnog nosača na Winklerovoj podlozi, za sastav tla definisan pod tačkom a) odnosno b).

Dimenzije temeljnog nosača su: $L = \underline{\hspace{2cm}}$ m, $B = \underline{\hspace{2cm}}$ m.

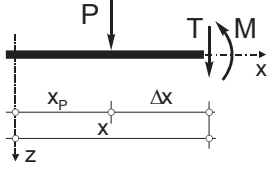
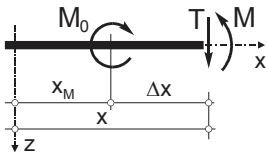
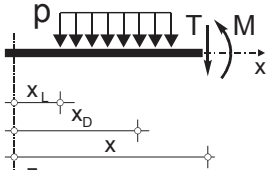
2. ZADATAK

Armirano betonski temeljni nosač datih dimenzija prema skici, dimenzionisati kao gredu na elastičnoj podlozi. Simulaciju podloge izvršiti Winklerovim modelom. Temeljno tlo ispod nosača je homogenog sastava do dubine oko 6.0m od površine terena.

Koristeći analitičko rešenje diferencijalne jednačine grede na Winklerovoj podlozi, potrebno je izračunati moment savijanja M , transverzalnu silu T , ugib (sleganje) w i kontakti napon (reaktivno opterećenje) u tačkama 1, 2 i 3 temeljnog nosača.



Tabelarni prikaz uticaja (M , T , w , θ) u preseku beskonačne grede na Winklerovoj podlozi

| Tip opterećenja: | Presečne sile $M(x)$ i $T(x)$, ugib $w(x)$ i nagib $\theta(x)$ | |
|--|---|---|
| | $\text{sgn}(\Delta x < 0) = -1$, $\text{sgn}(\Delta x = 0) = 0$, $\text{sgn}(\Delta x > 0) = 1$ | |
|  | $\Delta x = x - x_p$ | |
| | $M = \frac{P}{4\lambda} C(\lambda \Delta x)$ | $w = \frac{P\lambda}{2Bk} A(\lambda \Delta x)$ |
| $T = -\text{sgn}(\Delta x) \frac{P}{2} D(\lambda \Delta x)$ | $\theta = -\text{sgn}(\Delta x) \frac{P\lambda^2}{Bk} B(\lambda \Delta x)$ | |
|  | $\Delta x = x - x_M$ | |
| | $M = \text{sgn}(\Delta x) \frac{M_0}{2} D(\lambda \Delta x)$ | $w = \text{sgn}(\Delta x) \frac{M_0\lambda^2}{Bk} B(\lambda \Delta x)$ |
| $T = -\frac{M_0\lambda}{2} A(\lambda \Delta x)$ | $\theta = \frac{M_0\lambda^3}{Bk} C(\lambda \Delta x)$ | |
|  | $\Delta x_l = x - x_l$ | $\Delta x_d = x - x_d$ |
| | $M = \frac{P}{4\lambda^2} [\text{sgn}(\Delta x_l) \cdot B(\lambda \Delta x_l) - \text{sgn}(\Delta x_d) \cdot B(\lambda \Delta x_d)]$ | |
| | $T = \frac{p}{4\lambda} [C(\lambda \Delta x_l) - C(\lambda \Delta x_d)]$ | |
| | $w = \frac{p}{2Bk} [\text{sgn}(\Delta x_l) - \text{sgn}(\Delta x_d) - \text{sgn}(\Delta x_l) \cdot D(\lambda \Delta x_l) + \text{sgn}(\Delta x_d) \cdot D(\lambda \Delta x_d)]$ | |
| | $\theta = \frac{p\lambda}{2Bk} [A(\lambda \Delta x_l) - A(\lambda \Delta x_d)]$ | |

$$\lambda = \sqrt[4]{\frac{kB}{4E_b I_b}}$$

$$A(\lambda x) = e^{-\lambda x} [\cos(\lambda x) + \sin(\lambda x)]$$

$$B(\lambda x) = e^{-\lambda x} [\sin(\lambda x)]$$

$$C(\lambda x) = e^{-\lambda x} [\cos(\lambda x) - \sin(\lambda x)]$$

$$D(\lambda x) = e^{-\lambda x} [\cos(\lambda x)]$$

